

## Accepted Manuscript

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PII: S0955-2219(17)30766-5  
DOI: <https://doi.org/10.1016/j.jeurceramsoc.2017.11.027>  
Reference: JECS 11573

To appear in: *Journal of the European Ceramic Society*

Received date: 23-8-2017  
Revised date: 9-11-2017  
Accepted date: 10-11-2017

Please cite this article as: Varghese Jobin, Siponkoski Tuomo, Nelo Mikko, Sebastian Mailadil Thomas, Jantunen Heli. Microwave Dielectric Properties of Low-Temperature Sinterable  $\alpha$ -MoO<sub>3</sub>. *Journal of The European Ceramic Society* <https://doi.org/10.1016/j.jeurceramsoc.2017.11.027>

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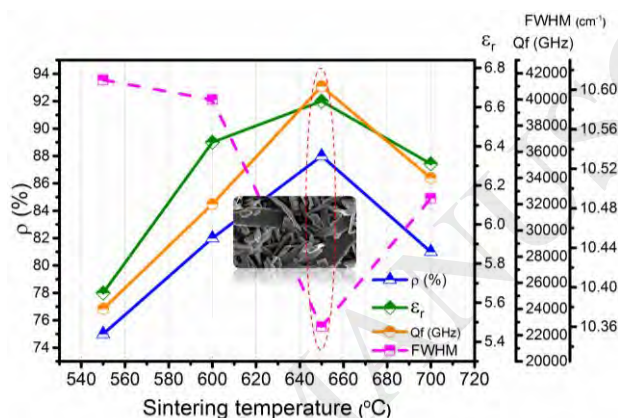
# Microwave Dielectric Properties of Low-Temperature Sinterable $\alpha$ -MoO<sub>3</sub>

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## TOC Graph

**TOC Synopsis:** Raman spectrum, low temperature sintering and high quality factor  $\alpha$ -MoO<sub>3</sub> binary ceramics



## Abstract

The  $\alpha$ -MoO<sub>3</sub> ceramics were prepared by uniaxial pressing and sintering of MoO<sub>3</sub> powder at 650 °C and their structure, microstructure, densification and sintering and microwave dielectric properties were investigated. The sintering temperature of  $\alpha$ -MoO<sub>3</sub> was optimized based on the best densification and microwave dielectric properties. After sintering at 650 °C the relative permittivity was found to be 6.6 and the quality factor was 41,000 GHz at 11.3 GHz. The full-width half-maximum of the A<sub>1g</sub> Raman mode of bulk  $\alpha$ -MoO<sub>3</sub> at different sintering temperatures correlated well with the Qf values. Moreover, the sintered samples showed a temperature coefficient of the resonant frequency of -25 ppm/°C in the temperature range from -40 to 85 °C and they exhibited a very low coefficient of thermal expansion of  $\pm 4$  ppm/°C. These microwave dielectric properties of  $\alpha$ -MoO<sub>3</sub> will be of great benefit in future MoO<sub>3</sub> based materials and their applications.

**Keywords:** Microwave Ceramics; Sintering; Raman Spectroscopy; X-ray photoelectron spectroscopy and Scanning electron microscopy

## Introduction

Molybdenum oxide ( $\text{MoO}_3$ ), because of its exceptional properties, has been the subject of much revived interest as a promising candidate for a broad range of applications such as catalysis [1,2], batteries [3, 4], supercapacitors [5], photo and electrochromic devices [6, 7], gas sensors [8], memory devices [9], organic light emitting diodes (OLEDs) [10], Dielectric/insulation applications [11], oxide solar cells [12], etc.  $\text{MoO}_3$  has four polymorph modifications, which include  $\alpha$ - $\text{MoO}_3$  (orthorhombic),  $\beta$ - $\text{MoO}_3$  (monoclinic), high-pressure  $\text{MoO}_3$ -II and h- $\text{MoO}_3$  (hexagonal). Among these, the  $\alpha$ - $\text{MoO}_3$  is a stable polymorph with a bilayer of distorted octahedra having excellent physical properties [13]. It has also been studied in the form of thin films, nanobelts, and nanorods[14-17].

The fast-growing wireless communication networks require ultra-low sintering temperature materials with excellent dielectric properties in the microwave frequency range. In addition, these materials further reduce the cost of production of a range of communication and consumer electronic products. The recent review of Ultra-Low Temperature Co-fired Ceramic (ULTCC) materials with sintering temperatures below  $700^\circ\text{C}$  by Sebastian *et. al.* [18], shows that most of the reported compositions are based on ternary molybdate based ceramics with relative permittivity ranging from 4.1 to 50 and Qf from 1,450 to 108,000 GHz [18,]. Some of the reported molybdate based ULTCC materials are  $\text{Na}_2\text{MoO}_4$  ( $\epsilon_r = 4.1$ , Qf = 35,000 GHz,  $\tau_f = -76$  ppm/ $^\circ\text{C}$ ) [19],  $\text{Li}_2\text{MoO}_4$  ( $\epsilon_r = 5.5$ , Qf = 46,000 GHz,  $\tau_f = -160$  ppm/ $^\circ\text{C}$ ) [20],  $\text{K}_2\text{Mo}_4\text{O}_{13}$  ( $\epsilon_r = 6.8$ , Qf = 39,800 GHz,  $\tau_f = -67$  ppm/ $^\circ\text{C}$ ) [21],  $\text{Sm}_2\text{Mo}_4\text{O}_{15}$  ( $\epsilon_r = 10.7$ , Qf = 63,500 GHz,  $\tau_f = -50$  ppm/ $^\circ\text{C}$ ) [22],  $\text{Te}_2\text{MoO}_7$  ( $\epsilon_r = 13.6$ , Qf = 46,900 GHz,  $\tau_f = -36$  ppm/ $^\circ\text{C}$ ) [23],  $\text{Pb}_2\text{MoO}_5$  ( $\epsilon_r = 19.1$ , Qf = 21,800 GHz,  $\tau_f = -215$  ppm/ $^\circ\text{C}$ ) [24] and  $\text{PbMoO}_4$  ( $\epsilon_r = 26.7$ , Qf = 42,800 GHz,  $\tau_f = 6$  ppm/ $^\circ\text{C}$ ) [25]. However, there are only a few reports of binary ceramics with low sintering temperatures and low dielectric loss at microwave frequency ranges. According to the ULTCC review, there are only two binary ceramic

materials ( $\text{TeO}_2$  and  $\text{Bi}_2\text{O}_3$ ) reported with firing temperature less than  $700^\circ\text{C}$ . The  $\text{TeO}_2$  ceramic is reported to have a low sintering temperature of  $640^\circ\text{C}/15\text{h}$  with  $\epsilon_r$  of 19.3,  $Q_f$  of 30,000 GHz and  $\tau_f$  of -119 ppm/ $^\circ\text{C}$  [18]. Similarly,  $\text{Bi}_2\text{O}_3$  ceramic was sintered at  $680^\circ\text{C}$  with  $\epsilon_r$  of 33.5,  $Q_f$  of 18,700 GHz and  $\tau_f$  of -235 ppm/ $^\circ\text{C}$  [18].

Recently, Vidya *et. al.*, in 2015 reported that  $\text{MoO}_3$  nanorod ceramics prepared by wet chemical synthesis are suitable for Low-Temperature Co-fired Ceramic (LTCC) and optical applications [26] with a relative permittivity of 8.01 and dielectric loss tangent of 0.02 at 5 MHz after sintering at  $700^\circ\text{C}$ . However, the microwave dielectric properties of  $\text{MoO}_3$  ceramics have not yet been reported. In this present paper the structural stability of sintered  $\alpha$ - $\text{MoO}_3$  ceramics along with their microwave dielectric properties are studied. The paper also demonstrates the exact correlation between the  $Q_f$  and Full Width Half Maximum (FWHM) value of the Raman spectrum for samples sintered at various temperatures.

## Experimental

$\text{MoO}_3$  bulk samples were prepared by simple solid state sintering and uniaxial pressing from high purity reagent grade  $\text{MoO}_3$  (> 99 %, Alfa Aesar). The powder was sieved to an average particle size of  $45\ \mu\text{m}$  and, for microwave measurements, was pressed into circular disks (diameter 10 mm and thickness 5 mm) with a uniaxial pressure using 50 MPa. Green samples were sintered in the temperature range of  $550$ - $700^\circ\text{C}$ . The crystal structure of the specimens was analyzed by X-ray diffractometer (D8, Bruker, Billerica, MA) using  $\text{Cu K}\alpha$  radiation. **A Thermo Fisher Scientific, ESCALAB 250 Xi using the  $\text{MgK}\alpha$  X-ray source was used for XPS analysis. Reference energies of Au  $4f_{5/2}$  ( $83.9\pm 0.1\ \text{eV}$ ) and Cu  $2p_{3/2}$  ( $932.7\pm 0.1\ \text{eV}$ ) were used for calibrating the spectrometer. The take-off angle (the angle between the surface and the analyzer) was kept at  $90^\circ$  for the measurement. A binding energy of  $285.0\ \text{eV}$  was assigned to the C 1s peak corresponding to the surface contamination and was used as an internal reference for the correction of charging effects. The energy resolution of the XPS is  $0.45$**

eV. Thermogravimetric (TG) and differential scanning calorimetric (DSC) analysis were carried out using TGA/DTA (NETZSCH, STA 499 F3 Jupiter, Germany) at a heating rate of 2 °C/min in air. The microstructure analysis of the MoO<sub>3</sub> was performed using scanning electron microscopy (FESEM, ZEISS Ultra Plus, Germany). The optical Raman spectra of the ceramic were measured with signals excited by a 488 nm Ar<sup>+</sup> laser using a spectrometer (LabRam HR800, Horiba Jobin-Yvon, Villeneuve-d'Arcy, France). The bulk densities of the sintered samples were measured by the Archimedes method. Relative permittivity, quality factor and temperature coefficient of resonant frequency were measured using Hakki Coleman and cavity methods connected to a vector network analyzer (10 MHz-20 GHz, ROHDE & SCHWARZ, ZVB20, Germany) and temperature chamber (SU-261, ESPEC CORP., Japan) in the temperature range of 25-85 °C. The temperature variation of relative permittivity and dielectric loss were measured using the Split Post Dielectric Resonator method operated at 9.97 GHz. **The total uncertainty of real permittivity did not exceed 0.5% and it was possible to resolve dielectric loss tangents to approximately  $5 \times 10^{-5}$  with the SPDR technique [27].** The coefficient of thermal expansion (CTE) was investigated in the temperature range of 25-500 °C with cylindrical samples of dimensions 8 mm × 15 mm using a dilatometer (NETZSCH, DIL 402 PC/4, Germany). The dilatometer measurement was performed at a heating rate of 5 °C/min. The temperature coefficient of resonant frequency ( $\tau_f$ ) was calculated using Equation 1 given below [28]. While  $f_{-40}$ ,  $f_{80}$  are initial and final resonant frequency similarly,  $T_{-40}$ ,  $T_{80}$  represents the initial and final measured temperatures.

$$\tau_f = \frac{f_{80} - f_{-40}}{f_{-40} * (T_{80} - T_{-40})} 10^{-6} \text{ ppm/}^\circ\text{C} \quad (1)$$

Porosity corrected relative permittivity was calculated using the modified Bruggeman correction for the two-phase system (solid and air) [28] and is shown in Equation 2, where  $P$  represents the porosity of the dielectric sample, air permittivity is taken as 1 to simplify the equation,  $\epsilon_{rc}$  is the porosity corrected

relative permittivity, and  $\epsilon_{rm}$  is the measured permittivity of the dielectric sample. This equation is more valid for the higher values of porosity [28].

$$\epsilon_{rc} = \frac{\epsilon_{rm}(3P-1-2\epsilon_{rm})}{3\epsilon_{rm}P-1-2\epsilon_{rm}} \quad (2)$$

The temperature coefficient of relative permittivity ( $\tau_\epsilon$ ) of the sample can be calculated using the equation [28].

$$\tau_\epsilon = -2(\tau_f + \alpha_L) \text{ ppm/}^\circ\text{C} \quad (3)$$

Where,  $\tau_f$  is temperature coefficient of resonant frequency from cavity method and  $\alpha_L$  is the linear coefficient of thermal expansion from dilatometer.

## Result and Discussions

Figure 1 (a) depicts the TG, DSC, and DDSC of the  $\text{MoO}_3$  ceramic sample from room temperature to 650  $^\circ\text{C}$ . From the TGA curve, the total mass loss of  $\text{MoO}_3$  ceramic was measured to be 0.018 %. The DSC and DDSC curves indicate that the sintering started at above 550  $^\circ\text{C}$ . The appearance of grain morphology before and after sintering is shown as optical and SEM images in the insets of Figure 1(a). Figure 1(b) depicts the X-ray diffraction pattern of  $\text{MoO}_3$  powder at room temperature (RT) and  $\text{MoO}_3$  after sintered at 650  $^\circ\text{C}$  indicating that they belonged to the stable phase. All the peaks are indexed based on the stable orthorhombic phase and the corresponding ICDD card no: 05-0508. It is reported that higher intensities of (0 k 0) planes with  $k = 2, 4$  and 6 reveal highly anisotropic grain growth of the oxides [29-31]. The  $\text{MoO}_3$  morphology during sintering has previously been well documented by various researchers and is also evident from the (0 k 0) planes present in the X-ray diffraction [14-17]. In  $\text{MoO}_3$  ceramics, highly distorted  $\text{MoO}_6$  octahedra, which are interconnected with the edges of the (001) plane and interlinked with the corner sharing (100) plane, lead to a double layer flake-like planar structure. This anisotropic grain growth in the flake-shaped  $\text{MoO}_3$  is common with stable  $\alpha\text{-MoO}_3$  [32-34]. In the present

case the XRD of the MoO<sub>3</sub> sintered at 650 °C had intense peaks for (0 k 0) planes such as (0 2 0), (0 4 0) and (0 6 0).

The oxidation behavior and chemical homogeneity of the MoO<sub>3</sub> ceramic were analyzed by the XPS technique. The MoO<sub>3</sub> ceramic sintered at 650 °C was used to analyze the spectrum within the surface layer of about 50 Å. The survey spectrum of the MoO<sub>3</sub> is shown in Figure 2 (a). Besides the expected Mo 3d, O 1s peaks, a low intense C 1s peak was also observed and is presented in the inset. The C 1s peak did not affect the interpretation of the present results and, in fact, was used for binding energy calibration by setting its binding energy at 284.8 eV for sample charging correction [35, 36]. All the unindexed peaks in the survey spectrum represent the other characteristic peaks and Auger peaks of Mo and O in the MoO<sub>3</sub> ceramic.

Figure 2 (b) shows the high-resolution spectrum of Mo 3d with spin-orbital splitting 3d<sub>5/2</sub> and 3d<sub>3/2</sub> having an orbital split of about 3.11 eV at a binding energy of 232.21 eV and 235.32 eV, respectively. The Mo 3d fitted binding energies have FWHM of 1.07 and 1.30 eV with atomic wt. % of 3.99 and 3.41 respectively. The Mo 3d scan suggests that Mo in MoO<sub>3</sub> ceramic sintered at 650 °C belongs to the 6<sup>+</sup> oxidation state [36]. It confirms that the MoO<sub>3</sub> sintered at 650 °C was stable. Core-level spectra of O 1s and its curve fitting for MoO<sub>3</sub> ceramic are shown in Figure 2 (c). This O 1s photoelectron peak provides information on the oxide ion in the sintered MoO<sub>3</sub> ceramics with Mo-O chemical bonding. A well-resolved peak at 530.15 eV fitted with atomic wt. % of 22.87 relates to the bridging oxygen atoms present in the MoO<sub>3</sub> ceramic. The peaks associated with Mo 3d as well as O 1s show good agreement with reported values [37, 38]. **The XPS results reveals, especially for Mo was stable at 6<sup>+</sup> oxidation state when it undergoes sintering at 650 °C, which confirm the stability of the MoO<sub>3</sub> after sintering process.**

Figure 3 (a) (b) (c) & (d) shows the microstructure of  $\text{MoO}_3$  sintered at 550, 600, 650 and 700 °C. The abnormal grain growth during sintering at 550-700 °C is clear from the SEM images. This abnormal grain growth restricted the densification for bulk  $\text{MoO}_3$  samples to some extent. However, the sample sintered at 650 °C (Figure 3 (c)), with fine, and long grains showed the highest densification of 88 %. On the other hand, the grains were smaller and more loosely packed after sintering at 550 and 600 °C. The sample sintered at 700 °C started to deform slowly due to the melting, sublimation and evaporation of  $\text{MoO}_3$ , hence exhibiting high porosity. It has been reported that above 700 °C the  $\text{MoO}_3$  vapor pressure is high and  $\text{MoO}_3$  slowly starts to evaporate at this temperature [39, 40].

Figure 4 (a) shows the Raman shift of bulk  $\text{MoO}_3$  sintered at 550, 600, 650 and 700 °C respectively.  $\alpha$ - $\text{MoO}_3$  belongs to the space group  $D_{2h}^{16}$ , having 16 atoms in the unit cell; four atoms of molybdenum and the remaining atoms are oxygen. According to group theory analysis, 48 vibrational modes are expected. Among these 48 vibrational modes, a total of 24 modes ( $8A_g + 8B_{1g} + 4B_{2g} + 4B_{3g}$ ) are Raman active modes [41-45]. The vibrational modes identified with  $\text{MoO}_3$  belong to the stretching, deformation and lattice modes. The Raman peaks at 996 and 821  $\text{cm}^{-1}$  are assigned to stretching  $A_g$  modes such as asymmetric stretching of  $\text{Mo=O}$  and doubly coordinated  $\text{Mo-O-Mo}$  (the corner shared oxygen present in the  $\text{MoO}_6$  octahedra) stretching modes respectively. The peak present at 666  $\text{cm}^{-1}$  belongs to the  $B_g$  mode assigned to triply coordinated oxygen stretching in the 3  $\text{MoO}_6$  [46]. These three main peaks are referred to as the fingerprint of stable  $\alpha$ - $\text{MoO}_3$  [47-49]. All the peaks and corresponding assigned modes in the Raman spectrum of bulk  $\text{MoO}_3$  sintered at 650 °C were well matched with previous reports in the literature as shown in Table 1. Among the vibration modes, the stretch mode ( $A_{1g}$  with wave number around 821  $\text{cm}^{-1}$ ) of the oxygen octahedra has the sturdiest polarity as well as the strongest intensity and hence exerts a strong impact on the microwave dielectric properties [41, 50, 51].



Figure 4 (b) represents the effect of the sintering temperature on densification, relative permittivity ( $\epsilon_r$ ), quality factor (Qf) and FWHM of the selected  $A_{1g}$  mode (high intensity as compared to other  $A_{1g}$  modes in the spectrum). The sintering experiments revealed that the densification increased to a maximum when sintered at 650 °C and after that showed a slight decrease, this being in line with the microstructural studies. Also, the relative permittivity and Qf of bulk  $\text{MoO}_3$  ceramics increased from 5.6 to 6.6 and from 24,000 to 41,000 GHz at 11.3 GHz, respectively, when the sintering temperature was increased from 550 °C to 650 °C. At the higher temperature of 700 °C, the densification, relative permittivity and Qf of the sample degraded. The porosity corrected relative permittivity of this ceramic was found to be 8 using equation 2 with a theoretical model for high porosity samples by the modified Bruggeman method [28].

The effect of sintering on the double co-ordinated Mo-O-Mo ordering of the ceramic was evident from analysis of the FWHM of the active mode in the Raman spectra. This Raman line exhibited no shift while the FWHM of bulk  $\text{MoO}_3$  ceramics varied with sintering temperature. From Figure 4 (b) it is clear that the FWHM decreased with increase in sintering temperature up to 650 °C and a further increase in sintering temperature resulted in an increase in FWHM. On the other hand, the Qf value followed the opposite trend (24,000 GHz to 41,000 GHz), and increased linearly with the decrease in FWHM, which is evident from Figure 4 (b). The bulk  $\text{MoO}_3$  ceramics sintered at 650 °C exhibited a minimum FWHM of the  $A_{1g}$  mode which indicated a high degree of ordering and low phonon damping which in turn leads to the higher value of Qf [52]. The decrease of FWHM denotes the weakening of the coherence and damping behavior of the  $A_{1g}$  stretching vibration and hence results in the reduction of anharmonic vibrations which in turn relates to low dielectric loss. It eventually leads to the increase in the intrinsic Qf value inversely [53-55]. However, it is noted that bulk  $\text{MoO}_3$  ceramics showed a good quality factor even at its relatively low densification of 88 % when sintered at 650 °C.

Figure 5 (a) shows the temperature (-40 – 85 °C) variation of Qf, and the resonant frequency of bulk MoO<sub>3</sub> ceramics sintered at 650 °C. It is noted that the highest Qf of 63,000 GHz was observed when the sample was at the measurement temperature of -40 °C and it gradually decreased on heating the sample to 85 °C. This is due to the lower phonon vibrations at sub-zero temperature. The resonant frequency also showed a similar trend. The bulk MoO<sub>3</sub> ceramics sample sintered at 650 °C showed a temperature coefficient of resonant frequency ( $\tau_f$ ) of -25 ppm/°C in the temperature range of -40 to 85 °C. *The sintered MoO<sub>3</sub> sample show linear coefficient of thermal expansion (CTE) of  $\pm 4$  ppm/°C measured in the temperature range of 25 to 500 °C. While, the CTE in the measured temperature range of 25 to 100 °C is about -2.7 ppm/°C. Based on the  $\tau_f$  and CTE value, the calculated  $\tau_\epsilon$  value is about 55 ppm/°C using the equation 3. The calculated  $\tau_\epsilon$  is positive and 2 time higher than the  $\tau_f$  and CTE of sintered MoO<sub>3</sub>. Figure 5 (b) shows the temperature variation of relative permittivity and dielectric loss of bulk MoO<sub>3</sub> ceramics sintered at 650 °C and measured using the SPDR technique at 9.97 GHz. It is evident from Figure 5 (b) that relative permittivity and dielectric loss slightly increased with temperature. The sintered MoO<sub>3</sub> substrate shows variation in permittivity upon heating (25 to 85 °C) is about 0.6 %. However, the observed microwave dielectric properties of MoO<sub>3</sub> will be of great interest for many applications.*

Table 2 shows the comparison of sintering temperature and microwave dielectric properties of low sintering binary ceramics with that of present work. It has been noted that, even with 88 % densification MoO<sub>3</sub> possess moderately high Qf of 41000 GHz and low temperature coefficient of resonant frequency of -25 ppm/°C in comparison with other binary oxide reported. However, it should be noted that most of the molybdates have a strong reaction with Ag and Al, which limits their usage with the commonly used Ag and Al electrodes in LTCC/ULTCC applications [see supporting information Figure S1]. It has been reported that Ag<sub>2</sub>MoO<sub>4</sub> and Al<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> are the major intermediate compounds when MoO<sub>3</sub> undergoes reaction with Ag and Al [56]. Still, the low temperature ( $\leq 200$  °C) commercial electrode DuPont 8453 may be used as post firing applications for the present binary MoO<sub>3</sub> [57]. In addition to that, most of the reported molybdates [19-25] are water-soluble like reported

H<sub>3</sub>BO<sub>3</sub>/B<sub>2</sub>O<sub>3</sub> microwave ceramics [58]. It has been reported that the binary MoO<sub>3</sub> water solubility is 0.490 g/100 mL (28 °C) in comparison with other ternary molybdates reported [59]. The importance of the present work is explore the excellent dielectric properties of the binary MoO<sub>3</sub> ceramics. The reported results will be a suitable reference for the potential growth in the various applications of stable MoO<sub>3</sub> ceramics.

## Conclusion

**The bulk  $\alpha$ -MoO<sub>3</sub> ceramics were prepared by uniaxial pressing and sintering.** This was followed by studies of the microstructure, densification, thermal and microwave dielectric properties. The XPS and Raman studies revealed the quality and quantity of the stable  $\alpha$ -MoO<sub>3</sub> ceramics developed. The optimized sintering temperature of MoO<sub>3</sub> ceramics obtained was 650 °C according to the highest densification and microwave dielectric properties. After sintering the measured relative permittivity was 6.6 and the quality factor (Qf) was 41,000 GHz at the resonance frequency of 11.3 GHz. The full-width half maximum (FWHM) of the A<sub>1g</sub> Raman mode of the bulk  $\alpha$ -MoO<sub>3</sub> ceramics at different sintering temperatures correlated well with the Qf values. The sintered samples showed a temperature coefficient of the resonant frequency of -25 ppm/°C in the temperature range of -40 to 85 °C. The sintered  $\alpha$ -MoO<sub>3</sub> ceramics showed a very low coefficient of thermal expansion of  $\pm 4$  ppm/°C measured in the temperature range of 25-500 °C. According to our best knowledge, this is the first time that the microwave dielectric properties of stable  $\alpha$ -MoO<sub>3</sub> ceramic have been reported.

## Acknowledgements

The authors are thankful to European Research Council Project No: 24001893 for financial support. Also, Mr. Santtu Heinilehto (Application Engineer) for XPS and Mr. Pekka Moilanen for Raman spectroscopy measurements are acknowledged.

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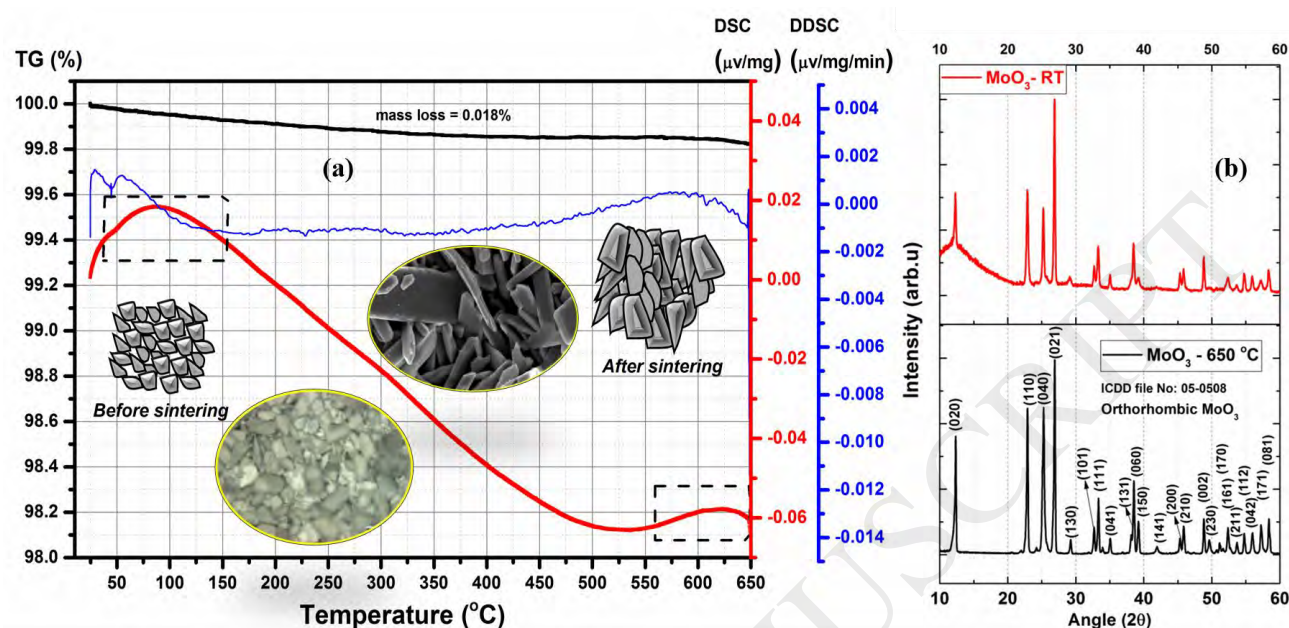


Figure 1. (a). TG, DSC and DDSC curve of  $\text{MoO}_3$  ceramic (inset figures show schematically the grain growth before and after sintering with supporting optical and SEM pictures ) and (b) X-ray diffraction pattern of  $\text{MoO}_3$  powder at room temperature and after sintering at 650  $^{\circ}\text{C}$ .

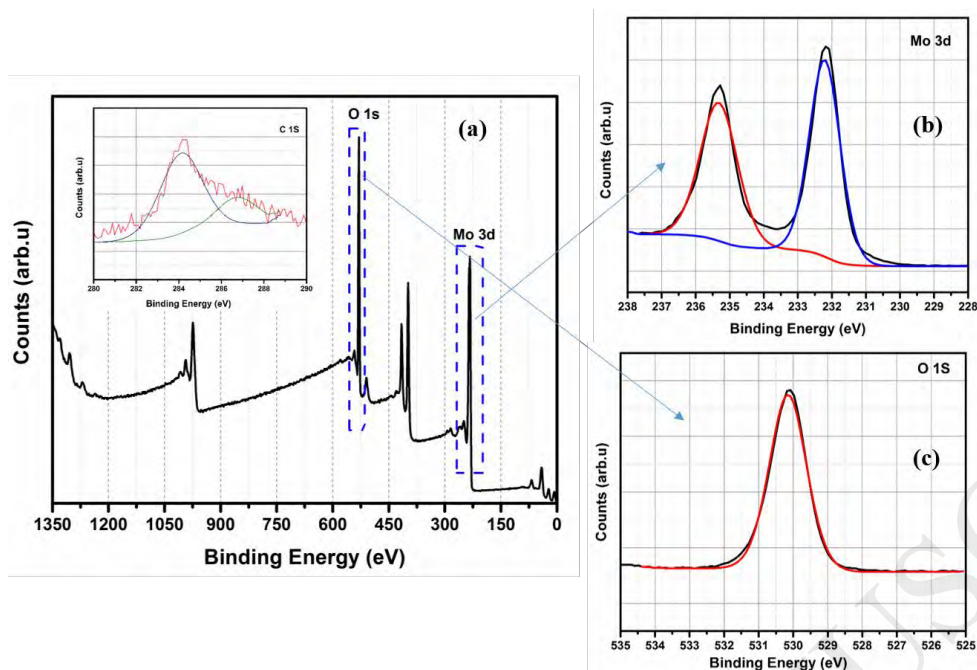


Figure 2 XPS analysis of  $\text{MoO}_3$  after sintering at  $650\text{ }^\circ\text{C}$  with (a) survey spectrum and inset figure high resolution carbon 1s peak, (b) fitted high resolution spectrum of Mo 3d and (c) fitted high resolution spectrum of O 1s.

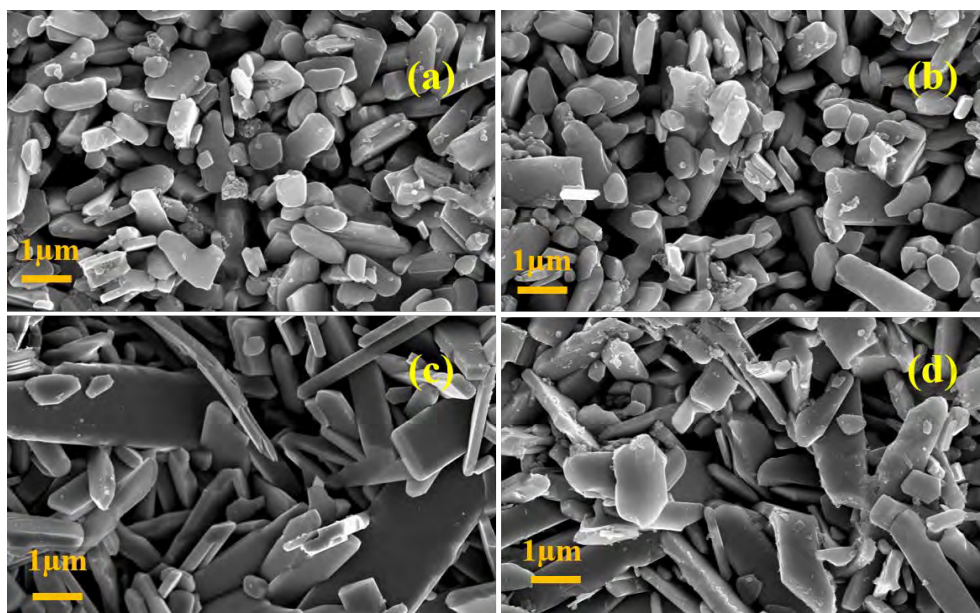


Figure 3 Microstructure of MoO<sub>3</sub> ceramic after sintering at (a) 550 °C, (b) 600 °C, (c) 650 °C and (d) 700 °C.

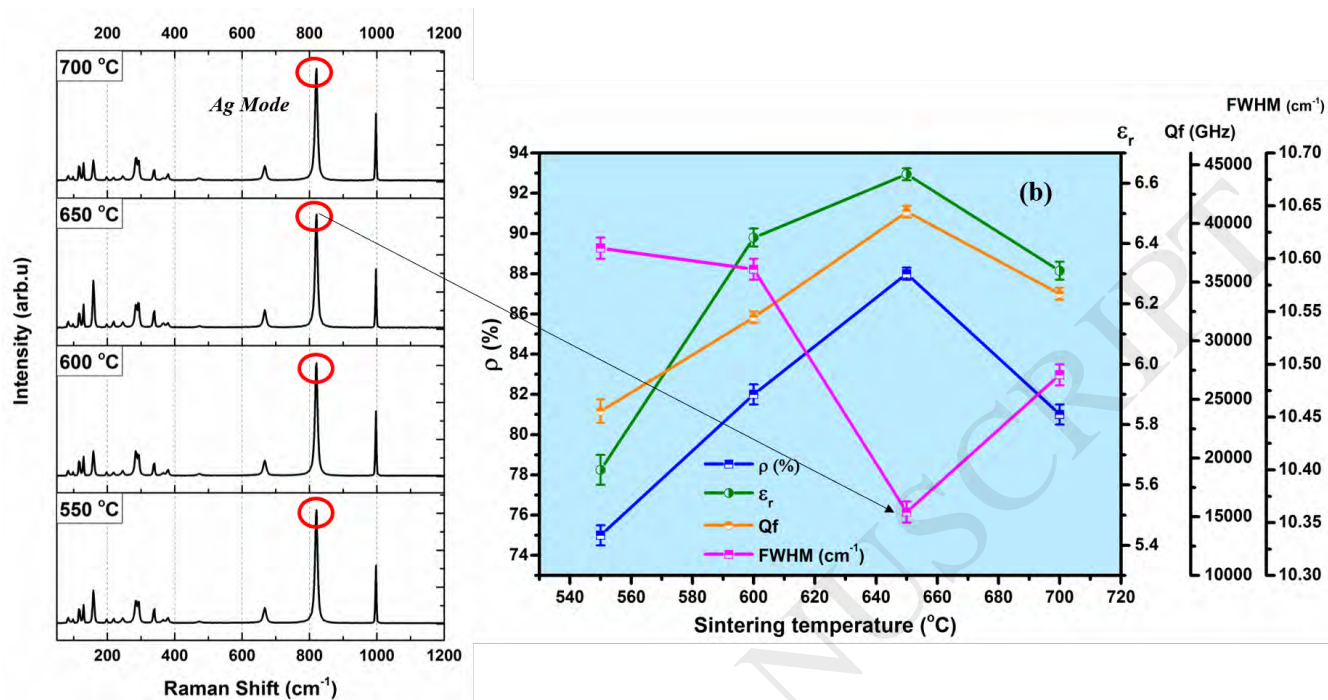


Figure 4 (a) Raman spectrum and (b) densification, relative permittivity,  $Q_f$  and full width half maximum of  $\text{MoO}_3$  sintered at various temperature.

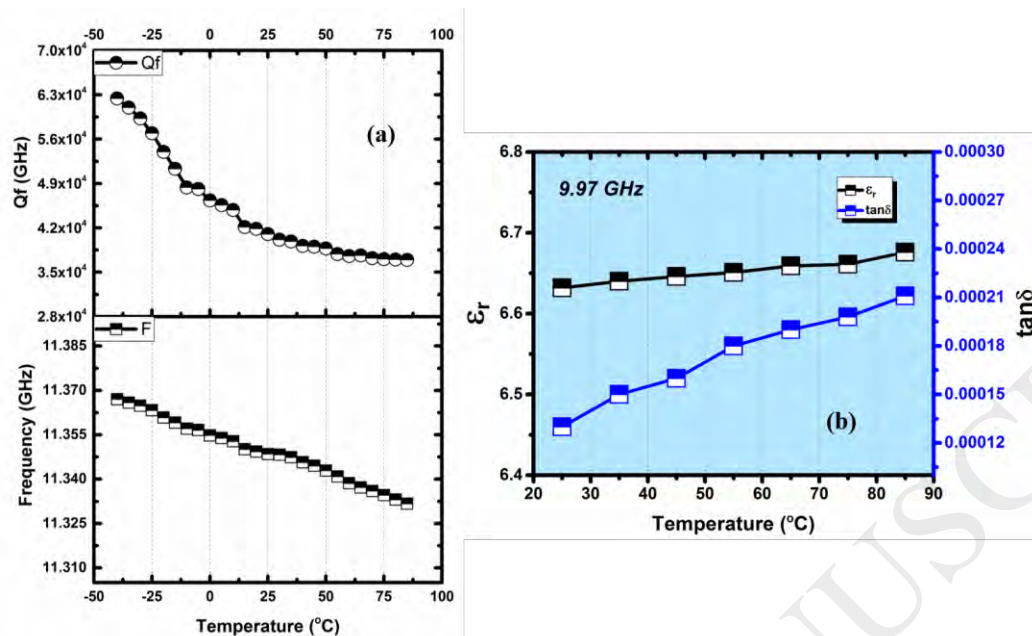


Figure 5 (a) Temperature variation of  $Q_f$  and resonant frequency and (b) temperature variation of relative permittivity and dielectric loss of bulk  $\text{MoO}_3$  ceramic sintered at  $650^\circ\text{C}$ .



Table 1 Raman mode assignments of bulk  $\text{MoO}_3$  ceramic sintered at 650 °C.

Raman shift ( $\text{cm}^{-1}$ )	Mode assignments Raman active - ( $8A_g + 8B_{1g} + 4B_{2g} + 4B_{3g}$ )	Reference based on previous reports
996	$A_g + B_{1g}$	41-49
819	$A_g + B_{1g}$	41-49
666	$B_{2g} + B_{3g}$	41-49
472	$A_g + B_{1g}$	41-49
381	$B_{1g}$	41-49
366	$A_g$	41-49
339	$A_g + B_{1g}$	41-49
283	$B_{2g} + B_{3g}$	41-49
246	$B_{3g}$	41-49
219	$A_g$	41-49
199	$B_{2g}$	41-49
160	$A_g + B_{1g}$	41-49
130	$B_{3g}$	41-49
118	$B_{2g}$	41-49
96	$B_{1g}$	41-49
83	$A_g$	41-49



Table 3 Comparison of sintering temperature microwave dielectric properties of low sintering temperature binary ceramics.

Composition	S.T <sup>&amp;</sup> (°C)	$\epsilon_r$	Qf (GHz)	$\tau_f$ (ppm/°C)	Ref.
TeO <sub>2</sub>	640	19.3	30000	-119	18
Bi <sub>2</sub> O <sub>3</sub>	680	33.5	18700	-235	18
H <sub>3</sub> BO <sub>3</sub> /B <sub>2</sub> O <sub>3</sub>	200	2.2	32700	-40	58
<b>MoO<sub>3</sub></b>	<b>650 (±5)</b>	<b>6.6 (±0.02)</b>	<b>41000 (±500)</b>	<b>-25 (±2)</b>	<b>Present work</b>

<sup>&</sup> S.T.: Sintering Temperature